

## WIND LOADING ANALYSIS - Main Wind-Force Resisting System

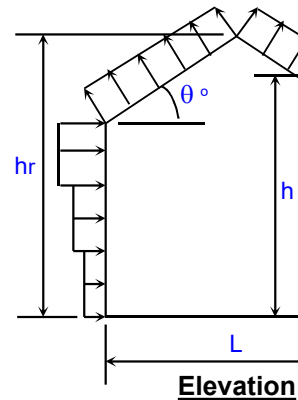
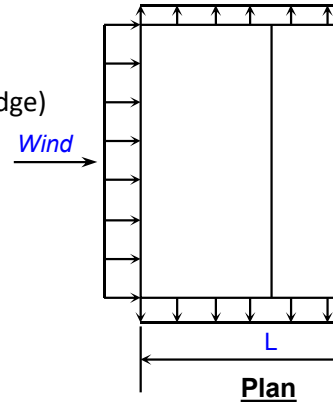
Per ASCE 7-05 Code for Enclosed or Partially Enclosed Buildings

Using Method 2: Analytical Procedure (Section 6.5) for Buildings of Any Height

Job Name:		Subject:	
Job Number:		Originator:	Checker:

### Input Data:

Wind Direction =	Normal	(Normal or Parallel to building ridge)
Wind Speed, V =	120	mph (Wind Map, Figure 6-1)
Bldg. Classification =	II	(Table 1-1 Occupancy Cat.)
Exposure Category =	B	(Sect. 6.5.6)
Ridge Height, hr =	157.00	ft. (hr >= he)
Eave Height, he =	157.00	ft. (he <= hr)
Building Width =	100.00	ft. (Normal to Building Ridge)
Building Length =	200.00	ft. (Parallel to Building Ridge)
Roof Type =	Monoslope	(Gable or Monoslope)
Topo. Factor, Kzt =	1.00	(Sect. 6.5.7 & Figure 6-4)
Direct. Factor, Kd =	0.85	(Table 6-4)
Enclosed? (Y/N)	Y	(Sect. 6.2 & Figure 6-5)
Hurricane Region?	N	
Damping Ratio, β =	0.030	(Suggested Range = 0.010-0.070)
Period Coef., Ct =	0.0200	(Suggested Range = 0.020-0.035) (Assume: $T = Ct \cdot h^{(3/4)}$ , and $f = 1/T$ )



### Resulting Parameters and Coefficients:

Roof Angle, θ =	0.00	deg.	
Mean Roof Ht., h =	157.00	ft. (h = he, for roof angle <=10 deg.)	
Windward Wall Cp =	0.80	(Fig. 6-6)	
Leeward Wall Cp =	-0.50	(Fig. 6-6)	
Side Walls Cp =	-0.70	(Fig. 6-6)	
Roof Cp (zone #1) =	-1.04	-0.18	(Fig. 6-6) (zone #1 for 0 to h/2)
Roof Cp (zone #2) =	-0.70	-0.18	(Fig. 6-6) (zone #2 for h/2 to h)
Roof Cp (zone #3) =	N.A.	N.A.	(Fig. 6-6) (zone #3 for h to 2*h)
Roof Cp (zone #4) =	N.A.	N.A.	(Fig. 6-6) (zone #4 for > 2*h)
+GCpi Coef. =	0.18	(Figure 6-5) (positive internal pressure)	
-GCpi Coef. =	-0.18	(Figure 6-5) (negative internal pressure)	

If  $z \leq 15$  then:  $K_z = 2.01 \cdot (15/z_g)^{(2/\alpha)}$ , If  $z > 15$  then:  $K_z = 2.01 \cdot (z/z_g)^{(2/\alpha)}$  (Table 6-3, Case 2)

$\alpha = 7.00$        $z_g = 1200$  (Table 6-2)

$K_h = 1.12$  (Kh = Kz evaluated at z = h)

$I = 1.00$  (Table 6-1) (Importance factor)

Velocity Pressure:  $q_z = 0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2 \cdot I$  (Sect. 6.5.10, Eq. 6-15)

$q_h = 35.23$  psf       $q_h = 0.00256 \cdot K_h \cdot K_{zt} \cdot K_d \cdot V^2 \cdot I$  (qz evaluated at z = h)

Ratio h/L = 1.570      freq., f = 1.127 hz.      (f >= 1, Rigid st)



- Notes: 1. (+) and (-) signs signify wind pressures acting toward & away from respective surfaces.  
 2. Per Code Section 6.1.4.1, the minimum wind load for MWFRS shall not be less than 10 psf.  
 3. References : a. ASCE 7-05, "Minimum Design Loads for Buildings and Other Structures".  
 b. "Guide to the Use of the Wind Load Provisions of ASCE 7-05"  
 by: Kishor C. Mehta and William L. Coulbourne (2010).  
 4. Roof zone #1 is applied for horizontal distance of 0 to h/2 from windward edge.  
 5. Roof zone #2 is applied for horizontal distance of h/2 to h from windward edge.

**Determination of Gust Effect Factor, G:**

Is Building Flexible?   $f \geq 1$  Hz.

**1: Simplified Method for Rigid Building**

G =

Parameters Used in Both Item #2 and Item #3 Calculations (from Table 6-2):

$\alpha^{\wedge}$ =	<input type="text" value="0.143"/>
$b^{\wedge}$ =	<input type="text" value="0.84"/>
$\alpha(\text{bar})$ =	<input type="text" value="0.250"/>
$b(\text{bar})$ =	<input type="text" value="0.45"/>
c =	<input type="text" value="0.30"/>
l =	<input type="text" value="320"/>
$\varepsilon(\text{bar})$ =	<input type="text" value="0.333"/>
z(min) =	<input type="text" value="30"/>

ft.  
ft.

Calculated Parameters Used in Both Rigid and/or Flexible Building Calculations:

z(bar) =	<input type="text" value="94.20"/>	= 0.6*h , but not < z(min) , ft.
lz(bar) =	<input type="text" value="0.252"/>	= c*(33/z(bar))^(1/6) , Eq. 6-5
Lz(bar) =	<input type="text" value="453.94"/>	= l*(z(bar)/33)^(ε(bar)) , Eq. 6-7
gq =	<input type="text" value="3.4"/>	(3.4, per Sect. 6.5.8.1)
gv =	<input type="text" value="3.4"/>	(3.4, per Sect. 6.5.8.1)
gr =	<input type="text" value="4.218"/>	= (2*(LN(3600*f)))^(1/2)+0.577/(2*LN(3600*f))^(1/2) , Eq. 6-9
Q =	<input type="text" value="0.805"/>	= (1/(1+0.63*((B+h)/Lz(bar))^0.63))^(1/2) , Eq. 6-6

**2: Calculation of G for Rigid Building**

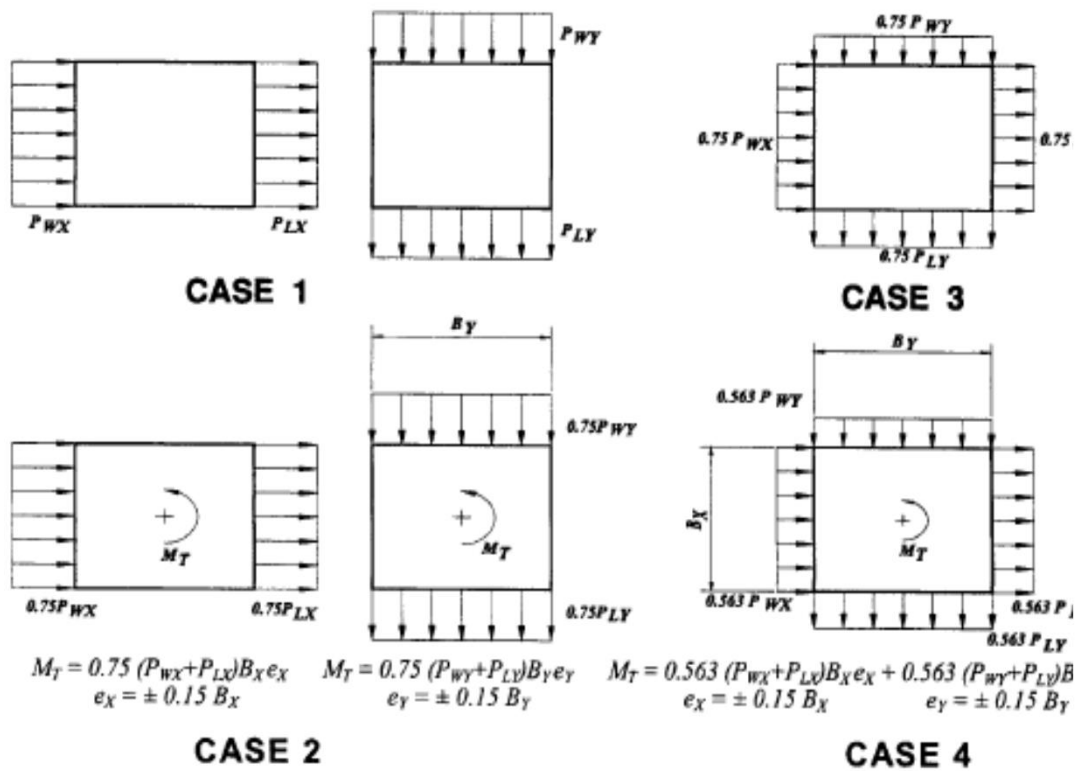
G =  = 0.925\*((1+1.7\*gq\*lz(bar)\*Q)/(1+1.7\*gv\*lz(bar))) , Eq. 6-4

**3: Calculation of Gf for Flexible Building**

$\beta$ =	<input type="text" value="0.030"/>	Damping Ratio
Ct =	<input type="text" value="0.020"/>	Period Coefficient
T =	<input type="text" value="0.887"/>	= Ct*h^(3/4) , sec. (Approximate fundamental period)
f =	<input type="text" value="1.127"/>	= 1/T , Hz. (Natural Frequency)
V(fps) =	<input type="text" value="N.A."/>	= V(mph)*(88/60) , ft./sec.

$V(\bar{v}, z\bar{v}) =$	N.A.	$= b(\bar{v}) * (z(\bar{v})/33)^{(\alpha(\bar{v}))} * V^*(88/60)$ , ft./sec., Eq. 6-14
$N1 =$	N.A.	$= f * Lz(\bar{v}) / (V(\bar{v}, z\bar{v}))$ , Eq. 6-12
$Rn =$	N.A.	$= 7.47 * N1 / (1 + 10.3 * N1)^{(5/3)}$ , Eq. 6-11
$\eta h =$	N.A.	$= 4.6 * f * h / (V(\bar{v}, z\bar{v}))$
$Rh =$	N.A.	$= (1/\eta h) - 1 / (2 * \eta h^2) * (1 - e^{-2 * \eta h})$ for $\eta h > 0$ , or $= 1$ for $\eta h = 0$ ,
$\eta b =$	N.A.	$= 4.6 * f * B / (V(\bar{v}, z\bar{v}))$
$RB =$	N.A.	$= (1/\eta b) - 1 / (2 * \eta b^2) * (1 - e^{-2 * \eta b})$ for $\eta b > 0$ , or $= 1$ for $\eta b = 0$ , E
$\eta d =$	N.A.	$= 15.4 * f * L / (V(\bar{v}, z\bar{v}))$
$RL =$	N.A.	$= (1/\eta d) - 1 / (2 * \eta d^2) * (1 - e^{-2 * \eta d})$ for $\eta d > 0$ , or $= 1$ for $\eta d = 0$ ,
$R =$	N.A.	$= ((1/\beta) * Rn * Rh * RB * (0.53 + 0.47 * RL))^{(1/2)}$ , Eq. 6-10
$Gf =$	N.A.	$= 0.925 * (1 + 1.7 * lz(\bar{v})) * (gq^2 * Q^2 + gr^2 * R^2)^{(1/2)} / (1 + 1.7$
Use: $G =$	0.818	

**Figure 6-9 - Design Wind Load Cases of MWFRS for Buildings of All Heights**



**Case 1:** Full design wind pressure acting on the projected area perpendicular to each principal axis

the structure, considered separately along each principal axis.

**Case 2:** Three quarters of the design wind pressure acting on the projected area perpendicular to each principal axis of the structure in conjunction with a torsional moment as shown, considered separately for each principal axis.

**Case 3:** Wind pressure as defined in Case 1, but considered to act simultaneously at 75% of the specified value. (Note: Load Case 3 would approximate "oblique" applied wind loading.)

**Case 4:** Wind pressure as defined in Case 2, but considered to act simultaneously at 75% of the specified value.

**Notes:** 1. Design wind pressures for windward ( $P_w$ ) and leeward ( $P_L$ ) faces shall be determined in accordance with the provisions of Section 6.5.12.2.1 and 6.5.12.2.3 as applicable for buildings of all heights.

2. Above diagrams show plan views of building.

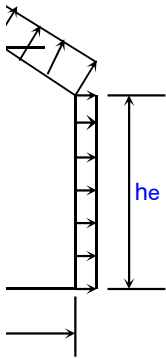
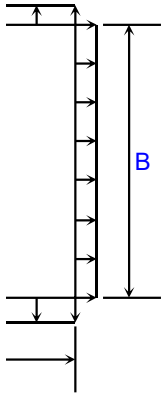
3. Notation:

$P_{wx}$ ,  $P_{wy}$  = Windward face pressure acting in the X, Y principal axis, respectively.

$P_{Lx}$ ,  $P_{Ly}$  = Leeward face pressure acting in the X, Y principal axis, respectively.

$e_x$ ,  $e_y$  = Eccentricity for the X, Y principal axis of the structure, respectively.

$M_T$  = Torsional moment per unit height acting about a vertical axis of the building.

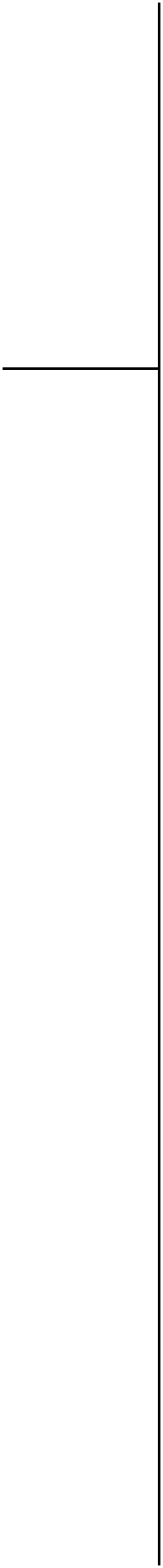


$L = 100 \text{ ft.}$   
 $B = 200 \text{ ft.}$

a)

(at  $z = h$ )  
structure)







,Eq. 6-13a,b

Eq. 6-13a,b

,Eq. 6-13a,b

\* $g_v \cdot l_z(\text{bar})$  ,  
Eq. 6-8

$P_{LX}$

$LX$

$l_y e_y$

of

each

ngs