| WIND LOADING ANALYSIS - Open Structures without Roofs | | | | | | |
|---|--------------------|-------------|--|----------|--|--|
| Per ASCE 7-05 Code | | | | | | |
| Using Method 2: Analytical Procedure (Section 6.5) for Other Structures of Any Height | | | | | | |
| Job Name: | Job Name: Subject: | | | | | |
| Job Number: | | Originator: | | Checker: | | |

Input Data:

| Wind Speed, V = | 90 | mph |
|--------------------------|--------|------------------------|
| Class., Occ. Category = | II | (Table 1-1) |
| Exposure Category = | С | (Sect. 6.5.6) |
| Topo. Factor, Kzt = | 1.00 | (Sect. 6.5.7) |
| Height of Structure, h = | 125.00 | ft. |
| Structure Width, B = | 150.00 | ft. (normal to wind) |
| Structure Length, L = | 100.00 | ft. (parallel to wind) |
| Damping Ratio, β = | 0.010 | (0.010 to 0.070) |
| Period Coefficient, Ct = | 0.0200 | (0.020 to 0.035) |
| Direct. Factor, Kd = | 0.85 | (Table 6-4) |
| Hurricane Region? | N | |
| | | |

<u>Note:</u> Per Code Section 6.1.4.1, design wind force for open buildings and other structures shall not be less than 10 psf multiplied by the area, 'Af', the area normal to wind direction.

Resulting Parameters and Coefficients:



Velocity Pressure (Sect. 6.5.10, Eq. 6-15): qz = 0.00256*Kz*Kzt*Kd*V^2*I Net Design Wind Pressures (Sect. 6.5.15): p = qz*G*Cf (psf), where 'qz' is evaluated at height 'z' of the centroid of projected area.

| | Open Structure - Net Design Wind Pressures, p | | | | | | | | |
|------------|---|------|-------|-------|-----------------------|-------|-------|-------|--|
| | | | | | Force Coefficient, Cf | | | | |
| | z | Kz | qz | qz*G | 1.20 | 1.60 | 1.80 | 2.00 | |
| | (ft.) | | (psf) | (psf) | р | р | р | р | |
| | | | | | (psf) | (psf) | (psf) | (psf) | |
| | 0 | 0.85 | 14.96 | 12.72 | 15.26 | 20.35 | 22.89 | 25.44 | |
| | 15 | 0.85 | 14.96 | 12.72 | 15.26 | 20.35 | 22.89 | 25.44 | |
| | 20 | 0.90 | 15.90 | 13.51 | 16.21 | 21.62 | 24.32 | 27.02 | |
| | 25 | 0.95 | 16.66 | 14.16 | 16.99 | 22.66 | 25.49 | 28.32 | |
| | 30 | 0.98 | 17.31 | 14.72 | 17.66 | 23.55 | 26.49 | 29.43 | |
| | 35 | 1.01 | 17.88 | 15.20 | 18.24 | 24.32 | 27.36 | 30.40 | |
| | 40 | 1.04 | 18.39 | 15.63 | 18.76 | 25.02 | 28.14 | 31.27 | |
| | 45 | 1.07 | 18.86 | 16.03 | 19.23 | 25.64 | 28.85 | 32.05 | |
| | 50 | 1.09 | 19.28 | 16.39 | 19.66 | 26.22 | 29.50 | 32.77 | |
| | 55 | 1.12 | 19.67 | 16.72 | 20.06 | 26.75 | 30.09 | 33.44 | |
| | 60 | 1.14 | 20.03 | 17.03 | 20.43 | 27.24 | 30.65 | 34.06 | |
| | 70 | 1.17 | 20.69 | 17.59 | 21.11 | 28.14 | 31.66 | 35.18 | |
| | 80 | 1.21 | 21.28 | 18.09 | 21.71 | 28.95 | 32.56 | 36.18 | |
| | 90 | 1.24 | 21.82 | 18.55 | 22.25 | 29.67 | 33.38 | 37.09 | |
| | 100 | 1.27 | 22.31 | 18.96 | 22.75 | 30.34 | 34.13 | 37.92 | |
| | 120 | 1.32 | 23.18 | 19.70 | 23.64 | 31.53 | 35.47 | 39.41 | |
| For z = h: | 125 | 1.33 | 23.38 | 19.87 | 23.85 | 31.80 | 35.77 | 39.75 | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

| Determination | of Gust Ef | fect Factor. G: | | | | | | |
|------------------------|---------------|--|---------------------------------|--------------|--------------------------|------------------|---------|--|
| | | | | | | | | |
| Flexible? | No | f >=1 Hz. | | | | | | |
| | | | | | | | | |
| 1: Simplified M | lethod for R | igid Structure | | | | | | |
| G = | 0.85 | | | | | | | |
| | | | | | | | | |
| Parameters U | Jsed in Both | Item #2 and Item | #3 Calculations | (from Table | 6-2): | | | |
| α^ = | 0.105 | | | | | | | |
| b^ = | 1.00 | | | | | | | |
| α (bar) = | 0.154 | | | | | | | |
| b(bar) = | 0.65 | | | | | | | |
| C = | 0.20 | | | | | | | |
| I = | 500 | ft. | | | | | | |
| ε(bar) = | 0.200 | | | | | | | |
| z(min) = | 15 | ft. | | | | | | |
| , , | | | | | | | | |
| Calculated Pa | arameters L | sed in Both Rigid a | nd/or Flexible S | tructure Cal | culations: | | | |
| z(bar) = | 75.00 | = 0.6*h . but not . | z(min) . ft. | | | | | |
| $I_{z(bar)} =$ | 0.174 | $= c^{*}(33/z(bar))^{(1/2)}$ | 6), Eq. 6-5 | | | | | |
| $I_z(bar) =$ | 589.22 | $= l^{(co)}(co)^{(co)}(co)^{(co)}$ | ar)). Eq. 6-7 | | | | | |
| gg = | 3.4 | (3.4. per Sect. 6.5. | 3.1) | | | | | |
| 84 øv = | 3.4 | (3.4 per Sect. 6.5 | R 1) | | | | | |
| gr = | 4 258 | $= (2^*(1 \text{ N}(3600^*\text{f})))^2$ | -(1/2)+0 577/(2* | LN(3600*f)) | ^(1/2) Ea f | 5-9 | | |
| 0 = | 0.848 | = (1/(1+0.63*)(B+t)) |)/I z(bar))^0 63) |)^(1/2) Fa | (1,2), <u>-</u> 9. (| | | |
| | 0.040 | | // L2(Bai)) 0.00) |) (1/2), ⊏9. | | | | |
| 2. Calculation | of G for Rigi | d Structure | | | | | | |
| L . calculation | 0.855 | = 0.925*((1+1.7*a)) | *lz(bar)*∩)/(1+ [,] | 1 7*av*lz(ba | r))) Eq. 6-4 | 1 | | |
| | 0.000 | 0.020 ((1.1.7.9) | | yv iz(ba | ·///, 느Ⴗ. 0 - | т | | |
| 3: Calculation | of Gf for Fle | xible Structure | | | | | | |
| | | Damping Patio | | | | | | |
| | 0.010 | Dariphing Rallo | | | | | | |
| | 0.020 | | (Poriod) | | | | | |
| | 1 227 | $= 1/T \Box_{-1}/A$ | | | | | | |
| | 1.337 NLA | $- \pm / 1$, $\pi 2$. (INALUI?) | ft (coo | | | | | |
| v(ips) = | IN.A. | = v(IIIµII) (88/80) = b(bar)*(z(bar)/22 | , 11./Set. \^(a(bar*\/*/09 | (60) ft /co | c Ea 6 14 | | | |
| | N.A. | = n(nai) (2(nai)/33) | $(u(uai)) \vee (00)$ | ,, ,, sec | o. , ∟q. 0-14 | | | |
| | IN.A. | | (Dar)), Eq. 6-12 | C 11 | | | | |
| Kn = | N.A. | $= 7.47^{1} N1/(1+10.3)$ | (5/3), Eq. | 0-11 | | | | |
| ηη = | N.A. | = 4.5"T"N/(V(bar,z | Jar)))*(1 o∧(0* b\\ → | formh > 0 | or = 1 for | Ь=0 Г ~ (| 6 120 h | |
| Rn = | N.A. | - (1/ηΠ)-1/(2¨ηΠ^2 | , (ι-e ⁻ (-2¨ηn)) | ιοιητι>υ, (| υ = ιτογη | $\Pi = U, Eq. t$ | 0-13a,D | |
| η ρ = | N.A. | = 4.6*t*B/(V(bar,z | par)) | | | | | |

| RB = | N.A. | = (1/ηb)-1/(2*ηb^2)*(1-e^(-2*ηb)) for ηb > 0, or = 1 for ηb = 0 , Eq. 6-13a,b |
|----------|-------|---|
| ηd = | N.A. | = 15.4*f*L/(V(bar,zbar)) |
| RL = | N.A. | = (1/ηd)-1/(2*ηd^2)*(1-e^(-2*ηd)) for ηd > 0, or = 1 for ηd = 0 , Eq. 6-13a,b |
| R = | N.A. | = ((1/β)*Rn*Rh*RB*(0.53+0.47*RL))^(1/2) , Eq. 6-10 |
| Gf = | N.A. | = 0.925*(1+1.7*lz(bar)*(gq^2*Q^2+gr^2*R^2)^(1/2))/(1+1.7*gv*lz(bar)), Eq. 6-8 |
| Use: G = | 0.850 | |
| | | - |

| Other Structu | ires - Method 2 | All Heights | | |
|---------------|--------------------|-------------------|------------------|--|
| Figure 6-22 | Force Coefficients | Open S | igns & | |
| | Cf | Lattice Fra | ameworks | |
| 3 | Flat-Sided | Rounded | Members | |
| | Members | D*SQRT(qz) <= 2.5 | D*SQRT(qz) > 2.5 | |
| < 0.1 | 2.0 | 1.2 | 0.8 | |
| 0.1 to 0.29 | 1.8 | 1.3 | 0.9 | |
| 0.3 to 0.7 | 1.6 | 1.5 | 1.1 | |

Notes: 1. Signs with openings comprising 30% or more of the gross area are classified as open signs.

- 2. The calculation of the design wind forces shall be based on the area of all exposed members and elements projected on a plane normal to the wind direction. Forces shall be assumed to act parallel to the wind direction.
- 3. The area 'Af' consistent with these force coefficients is the solid area projected normal to the wind direction.
- 4. Notation:
 - ϵ = ratio of solid area to gross area
 - D = diameter of a typical round member, in feet.
 - qz = velocity pressure evaluated at height 'z' above ground in psf.

| Other Structures - Method 2 | | All Heights | |
|-----------------------------|--------------------|----------------|--|
| Figure 6-23 | Force Coefficients | | |
| Cf | | Trussed Towers | |
| Open Structures | | | |
| | | | |
| Tower Cross Section | | Cf | |

| Square | 4.0*ε [^] 2 - 5.9*ε + 4.0 |
|----------|------------------------------------|
| Triangle | 3.4*ε^2 - 4.7*ε + 3.4 |

- <u>Notes:</u> 1. For all wind directions considered, area 'Af' consistent with force coefficients shall be solid area of tower face projected on plane of that face for tower segment under consideration.
 - 2. Specified force coefficients are for towers with structural angles or similar flat-sided members.
 - 3. For towers containing rounded member, it is acceptable to multiply specified force coefficients by following factor when determining wind forces on such members: $0.51 \epsilon^{2} + 0.57 \leq 1.0$.
 - 4. Wind forces shall be applied in directions resulting in maximum member forces and reactions. For towers with square cross-sections, wind forces shall be multiplied by following factor when wind is directed along a tower diagonal: $1+0.75^{*}\varepsilon \le 1.2$.
 - 5. Wind forces on tower appurtenances such as ladder, conduits, lights, elevators, etc., shall be calculated using appropriate force coefficients for these elements.
 - 6. Notation: ε = ratio of solid area to gross area of one tower face for segment considered.

Note: this worksheet DOES NOT address open structures with roofs!

Note: User is to input applicable values of Cf in table at left.

Use force coefficients, Cf,

from Figures 6-22 and 6-23.

User Input for Height, z (ft.):

| N | Use Input Values? |
|---|-------------------|
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For Flat Sided Members from Figure 6-22:





For Rounded Members from Figure 6-22:

| D = | 10.000 | ft. |
|---------------------|----------|------------------------------------|
| qz = | 25.00 | psf |
| Solid Area = | 6250.00 | ft.^2 |
| Gross Area = | 12500.00 | ft.^2 |
| Solidity Ratio, e = | 0.500 | ϵ = Solid Area/Gross Area |
| D*SQRT(qz) = | 50.00 | |
| Cf = | N.A. | Cf for D*SQRT(qz) <= 2.5 |
| Cf = | 1.1 | Cf for D*SQRT(qz) > 2.5 |
| Use: Cf = | 1.1 | Cf from Figure 6-22 |

| Solid Area = | 6250.00 | ft.^2 |
|------------------------------|----------|-------|
| Gross Area = | 12500.00 | ft.^2 |
| Solidity Ratio, ϵ = | 0.500 | |
| Square Tower Cf = | 2.05 | |
| Triangle Tower Cf = | 1.90 | |
| | | |

| ϵ = Solid Area/Gross Area |
|--|
| $Cf = 4.0^{*}\epsilon^{2} - 5.9^{*}\epsilon + 4.0$ |
| $Cf = 3.4 \epsilon^{2} - 4.7 \epsilon + 3.4$ |